

## HELLICALLY CORRUGATED WAVEGUIDE FILLED WITH PLASMA

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### Abstract

In this paper, we discuss the effect of plasma on helically corrugated waveguide. Specifically, the next section deals with synthesis of dispersion relation of helically corrugated waveguide completely filled with an ideal plasma.

### Introduction

Vacuum microwave tubes are the leading generators of electromagnetic energy for the applications in which medium or high power is required. Although conventional microwave tubes to be suitable for many of these applications, the performance of a large number of systems, which is determined by a combination of the bandwidth, efficiency, and microwave power, is limited by the capabilities of conventional vacuum microwave tubes. Research has showed that the presence of controlled amount of ionized gas (plasma) inside microwave tubes can improve the characteristic beyond what is currently available in evacuated devices. In particular, the presence of plasma can significantly increase the frequency bandwidth, operating efficiency, and power handling capabilities of microwave tubes and allow operation without a

expected to up shift the electromagnetic branches of the vacuum modes approximately as  $\omega_0^2 = \omega_p^2 + \omega^2$ , where  $\omega_0$  is the up shifted frequency of the plasma-filled circuit. It is observed that

guiding magnetic field. This can be attractive for systems and applications where size and weight are important [1-5].

Since a plasma consist of charged particles (electron and ions), it is subject to numerous natural oscillations in the microwave frequency range. For this reason, a device filled with plasma may serve as a source of microwave radiation.

The presence of the plasma changes both the beam propagation conditions and the electromagnetic properties of plasma filled tubes. Plasma influence on the electromagnetic characteristics of SWS's can be described by the parameter  $(\omega_p / \omega)$ , as long as the plasma density is not too high ( $\omega_p \leq \omega$ ). Here  $\omega_p$  and  $\omega$  are the electron plasma frequency and the frequency of the vacuum circuit mode. The plasma in this case is

plasma filling changes the electromagnetic properties of SWS in two manners: 1) the frequency of the electromagnetic modes is upshifted and 2) a plasma mode often referred to as the Trivelpiece-Gould mode is created [6-11]. The electrostatic modes of a plasma filled

periodic structure are quite complex and form a dense spectrum [12-13].

## 1.2 Dispersion relation of plasma filled helically corrugated waveguide

Consider a perfectly conducting helically corrugated waveguide completely filled with ideal electron plasma. The radius profile of the waveguide is similar to the chapter 2. Wall radius

$$R(z, \theta) = R_0 + h \cos(k_0 z + q_0 \theta) \quad (1)$$

Where  $k_0 = \frac{2\pi}{z_0}$  and  $q_0 = \frac{2\pi}{\varphi_1}$ .

Periodicity in axial direction is while periodicity in azimuthal direction is  $\varphi_1$ . Here  $R_0$  is the mean radius of the waveguide,  $h$  is the amplitude of the corrugation, and  $z_0$  is the corrugation period.

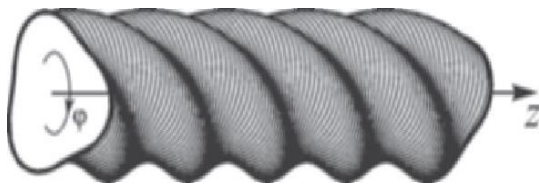


Fig1 Schematic view of a waveguide with a three-fold right-handed ( $q_0=3$ ) helical corrugation.

In case of plasma filled waveguide

$$\vec{\nabla} \times \vec{E} = \frac{i\omega}{c} \vec{B} \quad (2a)$$

$$\vec{\nabla} \times B = \frac{4\pi\vec{J}}{c} \vec{E} - \frac{i\omega}{c} \vec{E}$$

$$\vec{J} = \sigma \vec{E} \quad \text{and} \quad \sigma = \frac{i\omega_p^2}{4\pi\omega}$$

$$\vec{\nabla} \times B = -\frac{i\omega}{c} \left[ 1 - \frac{\omega_p^2}{\omega^2} \right] \vec{E}$$

$$\vec{\nabla} \times B = -\frac{i\omega}{c} \varepsilon \cdot \vec{E} \quad (2b)$$

Where  $\varepsilon = \left( 1 - \frac{\omega_p^2}{\omega^2} \right)$

Solving above equations (2a) and (2b) for transverse and axial components of electric and magnetic fields. Substituting the transverse components for  $E_z$  and  $B_z$  and rearranging the two equations we get the well known Bessel equation.

The solution of the equation representing axial fields is therefore

$$E_z = AJ_1(\beta r \sqrt{\varepsilon}) e^{i\varphi} \quad \text{and}$$

$$B_z = AJ_1(\beta r \sqrt{\varepsilon}) e^{i\varphi}$$

where

$$\varphi = -(\omega t - k_z z - l\theta)$$

Using above equations we can write

$$\vec{E} = \frac{e^{i\varphi}}{\beta^2} \begin{bmatrix} ik_z \beta \sqrt{\varepsilon} \frac{\partial}{\partial(\beta r \sqrt{\varepsilon})} J_l(\beta r \sqrt{\varepsilon}) A - \frac{lk}{r} J_l(\beta r) D \\ -\frac{lk_z}{r} J_l(\beta r \sqrt{\varepsilon}) A - ik\beta \frac{\partial}{\partial(\beta r)} J_l(\beta r) D \\ \beta^2 J_l(\beta r \sqrt{\varepsilon}) A \end{bmatrix} \quad (3a)$$

and

$$\vec{B} = \frac{e^{i\varphi}}{\beta^2} \begin{bmatrix} \frac{lk}{r} J_l(\beta r \sqrt{\varepsilon}) A + ik_z \beta \frac{\partial}{\partial \beta r} J_l(\beta r) D \\ ik\beta \sqrt{\varepsilon} \frac{\partial}{\partial \beta r \sqrt{\varepsilon}} J_l(\beta r \sqrt{\varepsilon}) - \frac{lk_z}{r} J_l(\beta r) D \\ \beta^2 J_l(\beta r) D \end{bmatrix} \quad (3b)$$

## FIELDS IN HELICAL WAVEGUIDE

Due to Floquet periodicity both in azimuthal as well as axial direction, we can write the azimuthal as well as axial fields as

$$\vec{E} = \sum_{n=-N}^{n=N} \sum_{p=-N}^{p=N} \frac{e^{i\theta_{np}}}{\beta_n^2} \begin{bmatrix} ik_{zn} \beta_n \sqrt{\varepsilon} \frac{\partial}{\partial \beta_n r \sqrt{\varepsilon}} J_{l_p}(\beta_n r \sqrt{\varepsilon}) A_{np} - \frac{l_p k}{r} J_{l_p}(\beta_n r) D_{np} \\ -\frac{l_p k_{zn}}{r} J_{l_p}(\beta_n r \sqrt{\varepsilon}) A_{np} - ik\beta_n \frac{\partial}{\partial \beta_n r} J_{l_p}(\beta_n r) D_{np} \\ \beta_n^2 J_{l_p}(\beta_n r \sqrt{\varepsilon}) A_{np} \end{bmatrix} \quad (4)$$

$$\vec{B} = \sum_{n=-N}^N \sum_{p=-N}^N \frac{e^{i\theta_{np}}}{\beta_n^2} \begin{bmatrix} \frac{l_p k}{r} J_{l_p}(\beta_n r \sqrt{\varepsilon}) A_{np} & ik_{zn} \beta_n \frac{\partial}{\partial \beta_n r} J_{l_p}(\beta_n r) D_{np} \\ ik\beta_n \sqrt{\varepsilon} \frac{\partial}{\partial(\beta_n r \sqrt{\varepsilon})} J_{l_p}(\beta_n r \sqrt{\varepsilon}) A_{np} & -\frac{l_p k_{zn}}{r} J_{l_p}(\beta_n r) D_{np} \\ & \beta_n^2 J_{l_p}(\beta_n r) D_{np} \end{bmatrix} \quad (5)$$

where

$$\varphi_{np} = -(\omega t - k_{zn} z - l_p \theta), \quad k_{zn} = k_z + nk_0 \quad \text{and} \quad l_p = l + pq_0$$

Here N is an integer tending to infinity.

## Boundary Conditions

$$E_z - hk_0 \sin(k_0 z + q_0 \theta) E_r \Big|_{R(z, \theta) = R_0 + h \cos(k_0 z + q_0 \theta)} = 0 \quad (6a)$$

$$E_\theta + \alpha \cos(k_0 z + q_0 \theta) E_\theta - q_0 \alpha \sin(k_0 z + q_0 \theta) E_r \Big|_{R(z, \theta) = R_0 + h \cos(k_0 z + q_0 \theta)} = 0 \quad (6b)$$

Where  $\alpha = \frac{h}{R_0}$

Substituting electric field components  $E_r, E_\theta$  from (4) in the first and second boundary conditions we get

$$\sum_{n=-N}^{n=N} \sum_{p=-N}^{p=N} \frac{e^{i(nu + p\delta)}}{\beta_n^2} \left\{ \begin{array}{l} \beta_n^2 J_{l_p}(\beta_n R \sqrt{\varepsilon}) A_{np} - \frac{hk_0 \beta_n}{2} \sin(u) \\ ik_{zn} \sqrt{\varepsilon} (J_{l_p-1}(\beta_n R \sqrt{\varepsilon}) - J_{l_p+1}(\beta_n R \sqrt{\varepsilon})) A_{np} \\ -k (J_{l_p-1}(\beta_n R) + J_{l_p+1}(\beta_n R)) D_{np} \end{array} \right\} = 0 \quad (7a)$$

$$\sum_{n=-N}^N \sum_{p=-N}^N \frac{e^{i(n+p\delta)}}{\beta_n^2} \left\{ \begin{array}{l} \frac{[1 + \alpha \cos(u)]}{2} \left[ k_{zn} \beta_n \sqrt{\varepsilon} (J_{l_p-1}(\beta_n R \sqrt{\varepsilon}) + J_{l_p+1}(\beta_n R \sqrt{\varepsilon})) A_{np} \right. \\ \left. + ik \beta_n (J_{l_p-1}(\beta_n R) - J_{l_p+1}(\beta_n R)) D_{np} \right] \\ \frac{q_0 \alpha}{2} \sin(u) \left[ ik_{zn} \beta_n \sqrt{\varepsilon} (J_{l_p-1}(\beta_n R \sqrt{\varepsilon}) - J_{l_p+1}(\beta_n R \sqrt{\varepsilon})) A_{np} \right. \\ \left. - k \beta_n (J_{l_p-1}(\beta_n R) + J_{l_p+1}(\beta_n R)) D_{np} \right] \end{array} \right\} = 0 \quad (7b)$$

## DISPERSION RELATION

$$\sum_{n=-N}^N \sum_{p=-N}^N \frac{4\pi}{\beta_n^2} \left\{ \begin{array}{l} \left[ \beta_n^2 R_{l_p}^{nm} - \frac{hk_0 \beta_n}{4} k_{zn} \sqrt{\varepsilon} (P_{l_p}^{nm-1} - P_{l_p}^{nm+1} - Q_{l_p}^{nm-1} + Q_{l_p}^{nm+1}) \right] A_{np} \\ - \frac{ihk_0 k \beta_n}{4} (H_{l_p}^{nm-1} - H_{l_p}^{nm+1} + L_{l_p}^{nm-1} - L_{l_p}^{nm+1}) D_{np} \end{array} \right\} \delta_{p-o-n+m,0} = 0 \quad (8)$$

$$-2\pi \sum_{n=-N}^N \sum_{p=-N}^N \frac{1}{\beta_n^2} \left\{ \begin{array}{l} \left[ k_{zn} \beta_n \sqrt{\varepsilon} (P_{l_p}^{nm} + Q_{l_p}^{nm}) + \frac{\alpha k_{zn} \beta_n \sqrt{\varepsilon}}{2} (P_{l_p}^{nm-1} + P_{l_p}^{nm+1} + Q_{l_p}^{nm-1} + Q_{l_p}^{nm+1}) \right. \\ \left. + \frac{q_0 \alpha}{2} k_{zn} \beta_n \sqrt{\varepsilon} (P_{l_p}^{nm-1} - P_{l_p}^{nm+1} - Q_{l_p}^{nm-1} + Q_{l_p}^{nm+1}) \right] A_{np} \\ + i \left[ k \beta_n (H_{l_p}^{nm} - L_{l_p}^{nm}) + \frac{\alpha k \beta_n}{2} (H_{l_p}^{nm-1} + H_{l_p}^{nm+1} - L_{l_p}^{nm-1} - L_{l_p}^{nm+1}) \right. \\ \left. + \frac{q_0 \alpha}{2} k \beta_n (H_{l_p}^{nm-1} - H_{l_p}^{nm+1} + L_{l_p}^{nm-1} - L_{l_p}^{nm+1}) \right] D_{np} \end{array} \right\} \delta_{p-o-n+m,0} = 0 \quad (9)$$

Equations (8) and(9), will give the dispersion relation

We denote

$$i = (2N + 1)[N + m] + N + o + 1$$

$$j = (2N + 1)[N + n] + N + p + 1,$$

Then (.9) and 10) can be written as

$$\sum_{j=1}^{(2N+1)(2N+1)} (T_{ij} G_j + U_{ij} K_j) = 0 \quad (10a)$$

and

$$\sum_{j=1}^{(2N+1)(2N+1)} (V_{ij} G_j + W_{ij} K_j) = 0 \quad (10b)$$

where

$$T_{ij} = \left[ R_{l_p}^{nm} - \frac{hk_0 k_{zn} \sqrt{\varepsilon}}{4\beta_n} (P_{l_p}^{nm-1} - P_{l_p}^{nm+1} - Q_{l_p}^{nm-1} + Q_{l_p}^{nm+1}) \right] \delta_{p-o-n+m,0} \quad (11a)$$

$$U_{ij} = \left[ -\frac{ihk_0 k}{4\beta_n} (H_{l_p}^{nm-1} - H_{l_p}^{nm+1} + L_{l_p}^{nm-1} - L_{l_p}^{nm+1}) \right] \delta_{p-o-n+m,0} \quad (11b)$$

$$V_{ij} = \frac{k_{zn} \sqrt{\varepsilon}}{\beta_n} \left[ \begin{array}{l} (P_{l_p}^{nm} + Q_{l_p}^{nm}) + \frac{\alpha}{2} (P_{l_p}^{nm-1} + P_{l_p}^{nm+1} + Q_{l_p}^{nm-1} + Q_{l_p}^{nm+1}) \\ + \frac{q_0 \alpha}{2} (P_{l_p}^{nm-1} - P_{l_p}^{nm+1} - Q_{l_p}^{nm-1} + Q_{l_p}^{nm+1}) \end{array} \right] \delta_{p-o-n+m,0} \quad (11c)$$

$$W_{ij} = \frac{ik}{\beta_n} \left[ \begin{array}{l} (H_{l_p}^{nm} - L_{l_p}^{nm}) + \frac{\alpha}{2} (H_{l_p}^{nm-1} + H_{l_p}^{nm+1} - L_{l_p}^{nm-1} - L_{l_p}^{nm+1}) \\ + \frac{q_0 \alpha}{2} (H_{l_p}^{nm-1} - H_{l_p}^{nm+1} + L_{l_p}^{nm-1} - L_{l_p}^{nm+1}) \end{array} \right] \delta_{p-o-n+m,0} \quad (11d)$$

Equation (10a) and (10b) are joined to a matrix form given by

$$\begin{bmatrix} T_{ij} & U_{ij} \\ V_{ij} & W_{ij} \end{bmatrix} \begin{bmatrix} G_j \\ K_j \end{bmatrix} = 0 \quad (12)$$

In order to have a nonzero set of  $G_j$  and  $K_j$ , the following determinant must be zero, namely

$$D(\omega, k) = \det \begin{bmatrix} T_{ij} & U_{ij} \\ V_{ij} & W_{ij} \end{bmatrix} = 0 \quad (13)$$

The required dispersion relation for helically corrugated waveguide can be given by the above matrix equation (14).

The value of  $T_{ij}$  and  $V_{ij}$  will change in comparison to the cold dispersion relation of HRW. Equation (13) is the relation of mean hybrid modes that have both rf axial magnetic and electric field components in the plasma filled helically corrugated waveguide with applied axial magnetic field of finite strength.

### Results

The result is that in contrast to the vacuum electromagnetic mode, hybrid modes with strongly increased amplitude of the axial component of the electric field near the axis of the SWS can occur, thus allowing a strong coupling. In plasma-filled device the interaction can involve both electromagnetic modes of the SWS and electrostatic modes supported by the plasma.

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