

## ENHANCING INDUCTION MOTOR PERFORMANCE WITH ADVANCED INVERTER TOPOLOGIES

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### ABSTRACT

The multilevel inverter fed induction motor drive is simulated and implemented in this research. Multilevel inverters lower the output harmonic content. In a symmetrical circuit, as the number of inverter levels increases, so do the voltage and power. To minimise harmonic distortion, the switching angle of the pulse is chosen. Higher torque and less overall harmonic distortion are two benefits of this drive system. PWM technique is used in the development of the multilayer inverter system model to regulate the induction motor. At these edges, the voltage change rate with respect to time, or  $dv/dt$ , is extraordinarily high, ranging from 500 to 5000 V/ $\mu$ s. While three-level inverter topology has drawn interest in high power, high performance voltage drive applications, two-level inverter topology has garnered attention in low power, low voltage drive applications. Low-range power applications are covered by single-phase VSI, whereas medium- to high-power applications are covered by three-phase VSI. The primary goal of these three-level inverter topologies is to supply a three-phase voltage source with constant adjustable amplitude, phase, and frequency. Despite the fact that the majority of applications demand sinusoidal voltage waveforms Key words: multilayer converter topologies, medium-voltage AC drivers

### 1. INTRODUCTION

Multilevel converters are considered for high-power medium-voltage drive applications, because the power structure can be realized with devices of lower voltage ratings [1]– [10]. A five-level inverter structure by cascading conventional two-level and three-level inverters is proposed in Part I of this paper [20]. An open-loop control scheme is presented in Part I to maintain dc-link capacitor voltage balancing and common-mode voltage (CMV) elimination in a dual five-level inverter-fed open-end winding induction motor (IM) drive, which effectively uses only the available redundant switching states of the inverter. It is pointed out that the proposed open loop controller is unable to take any corrective action to reduce the unbalance in the capacitor voltages that may arise. Every individual inverter is capable of generating three different voltage output  $+V_{dc}$ ,  $0$ ,  $-V_{dc}$  by connecting the dc source to the ac output side by different combinations of the four switches  $S_1$ ,  $S_2$ ,  $S_3$  and  $S_4$  [1]. The synthesized ac output voltage waveform of the sum of all the individual inverter's outputs. The number of output phase voltage level of cascade multilevel inverter is  $2s+1$  where  $S$  is the number of dc sources. This outstandingly increases the level number of the output wave form and thereby dramatically reduced to the low order harmonics and total harmonic distortion. One of the foremost motives for developing the multilevel inverter is to reduce cost. Similar voltage profiles can also be obtained by using higher order neutral-point-clamped (NPC) multilevel inverters or by cascading a number of two-level inverters. However, the multilevel NPC inverters suffer from dc-bus imbalance, device underutilization problems and unequal ratings of the clamped diodes, etc., which are not very serious problems for inverters with three levels or lower. The capacitor voltage imbalance for a five-level one is presented in which suggest the need of extra hardware in the form of dc choppers or a back-to-back connection of multilevel converters. The cascaded H-bridge topology suffers from the drawbacks of the usage of huge dc-bus capacitors and complex input transformers for isolated dc bus for each module. These drawbacks are addressed in the proposed topology. Furthermore, the power

circuit is modular in structure, and hence, the number of modules to be connected in series depends on the power of the drive.

## 2. PROPOSED CONVERTER TOPOLOGY

The proposed general configuration of “n” number of three level inverters connected in series is shown in Fig. 1. Each inverter module is a three-phase NPC three-level inverter. At the output stage, transformers are used to have the series connection of three-level inverters, as shown in Fig. 1. If “V<sub>dc</sub>” is the dc-bus voltage of each inverter module, then “α” is the turns ratio of each transformer and “n” is the number of inverter modules then for sine PWM (SPWM) strategy; the motor rms phase voltage (V<sub>Ph\_motor</sub>) can be expressed as follows  $Rms\ of\ V_{ph\_motor} = \sqrt{3} \alpha m V_{dc} / (2\sqrt{2})$  Where m is the modulation index of the inverter topology defined as follows  $m = (\text{Peak of } V_{(ph\_inverter)}) / (n V_{dc} / 2)$  V<sub>ph\_inverter</sub> is the total phase voltage reference of the inverter topology. For the given peak of V<sub>Ph\_motor</sub>, peak of V<sub>ph\_inverter</sub> can be computed as follows  $\text{Peak of } V_{(ph\_inverter)} = (\text{Peak of } V_{(ph\_motor)}) / (\sqrt{3} \alpha)$  The generation of individual reference voltage signal of each inverter is discussed as follows. The gate pulses for each three-level inverter module can be derived using two carrier signals. Thus, “n” numbers of such three-level inverter modules require “2n” number of carriers [10], [13]. The three-phase voltage reference signals are then compared with these carrier waves to produce the gate pulses for the inverters. For example, the carrier waves and the sinusoidal modulating voltage signal (SPWM technique) for R phase is shown in Fig. 2 for four series-connected three-level inverters. The carrier waves 1 and 1\_ (Fig. 2) with R-phase voltage reference controls the inverter module 1. Similarly, 2 2\_, 3-3\_, and 4-4\_ carrier waves with R-phase voltage reference generate the gate pulses for the three-level inverter modules 2, 3, and 4, respectively. Thus, each inverter module produces the voltage proportional to a part of the reference phase voltage signals. It is important to note that no two three-level inverter modules switch simultaneously. Thus, the maximum dv/dt rate of the output voltage of this topology is limited to that of a single three-level inverter module.

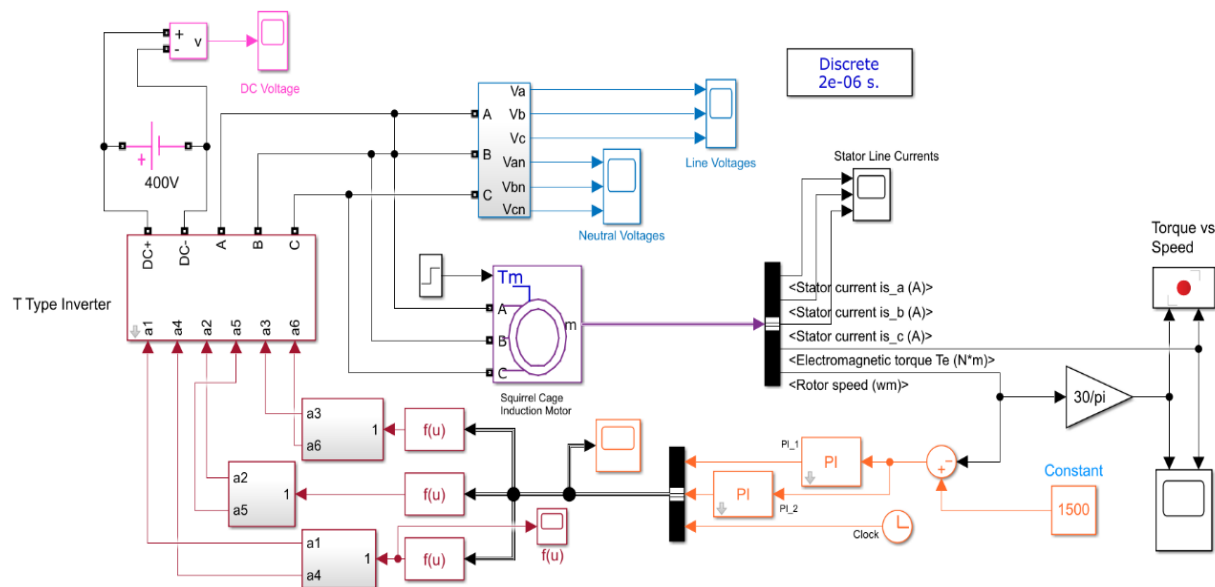
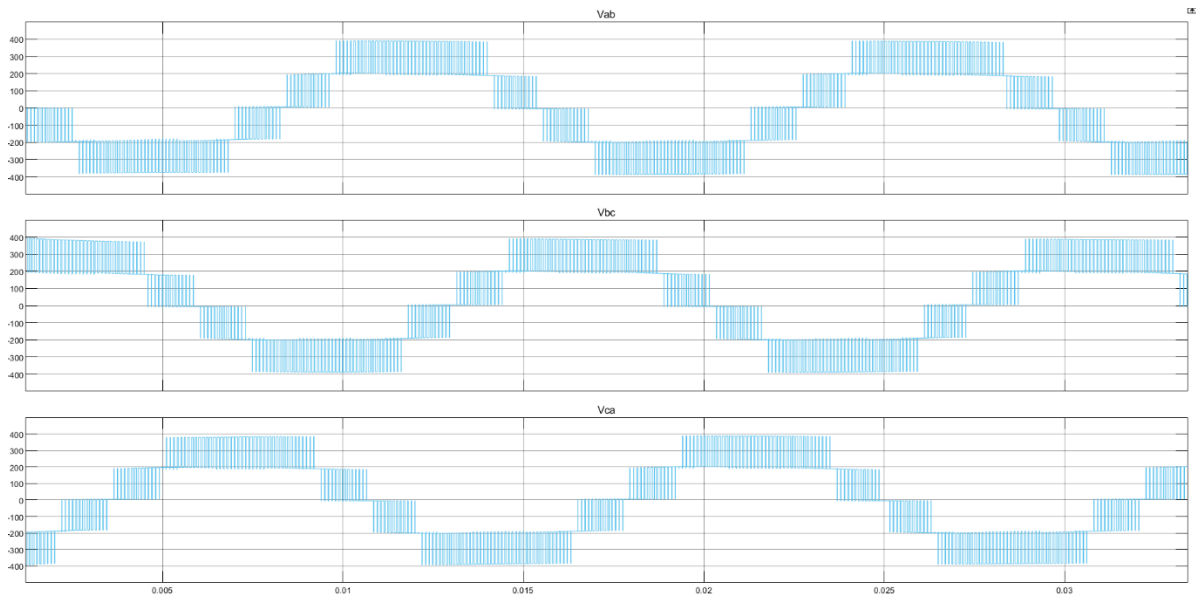


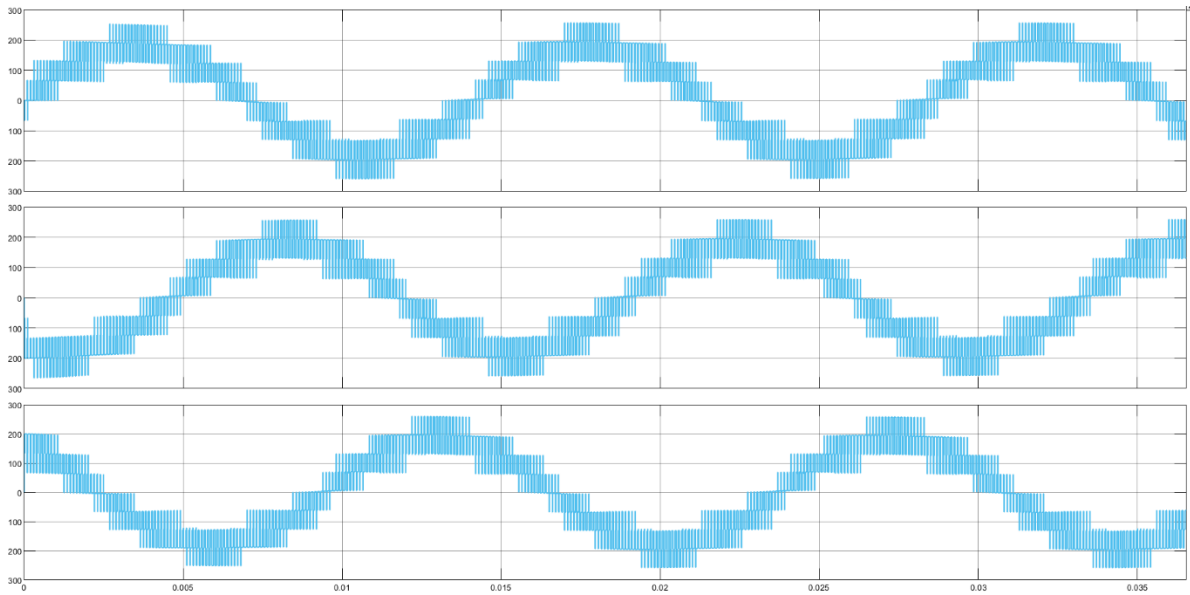
Fig 1 Proposed circuit configuration

**TABLE-I (SWITCHING TABLE)**

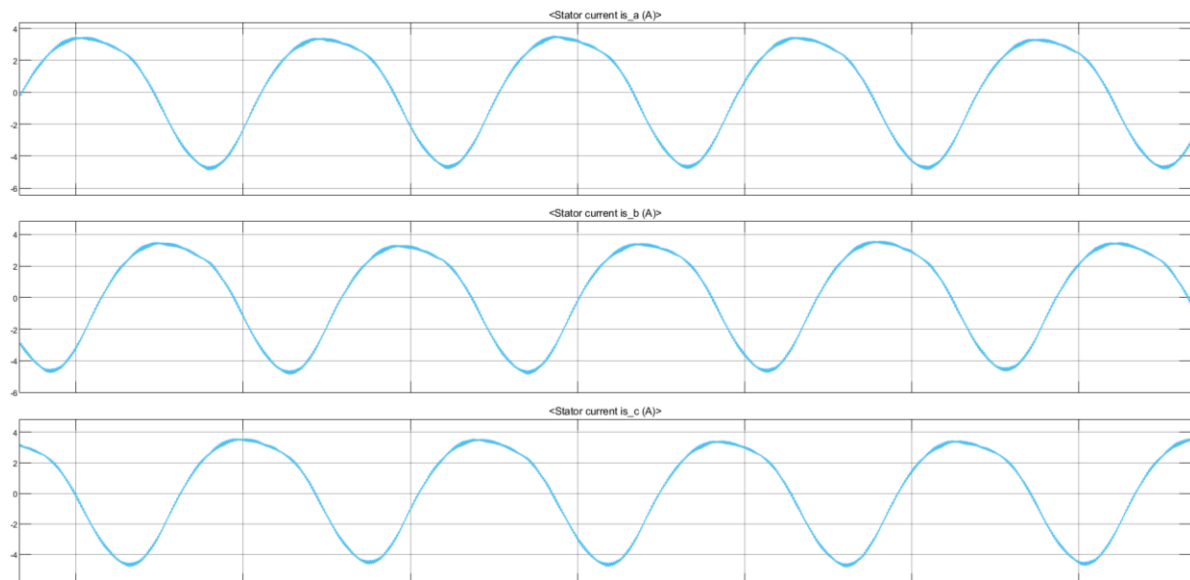
Generation of Level	Switching Devices				Output Voltage
	T1	T2	T3	T4	
<b>+Vdc/2</b>	on	off	On	off	+1v
<b>0</b>	off	on	On	off	0v
<b>-Vdc/2</b>	off	on	Off	on	-1v



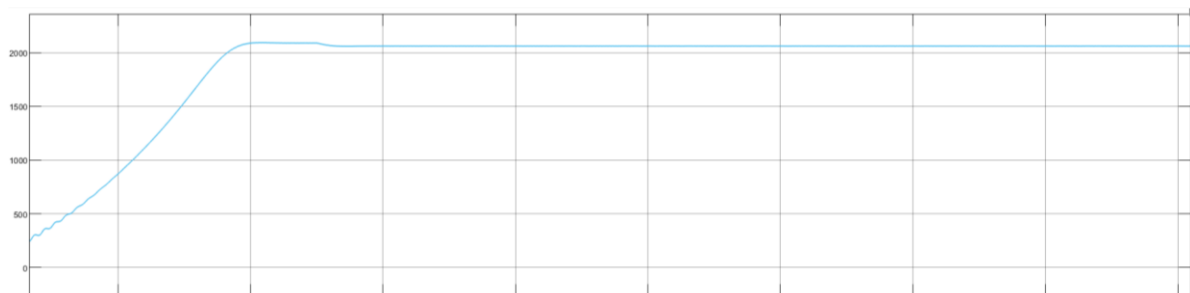
Neutral Voltages



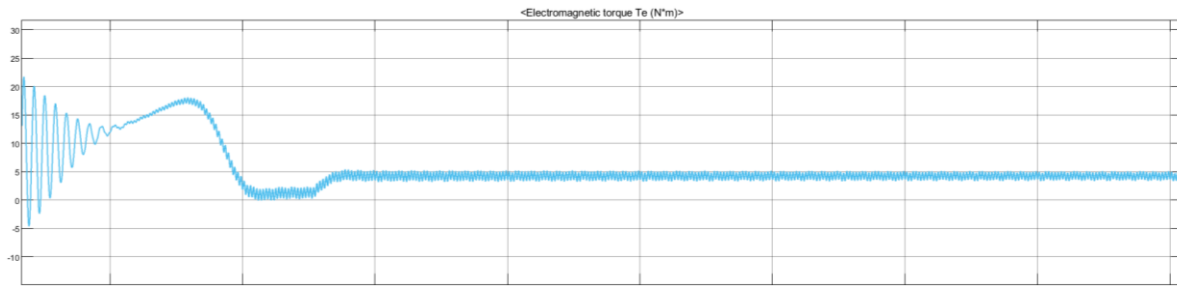
Stator Line Currents



Speed



Torque



No Load Torque vs Slip

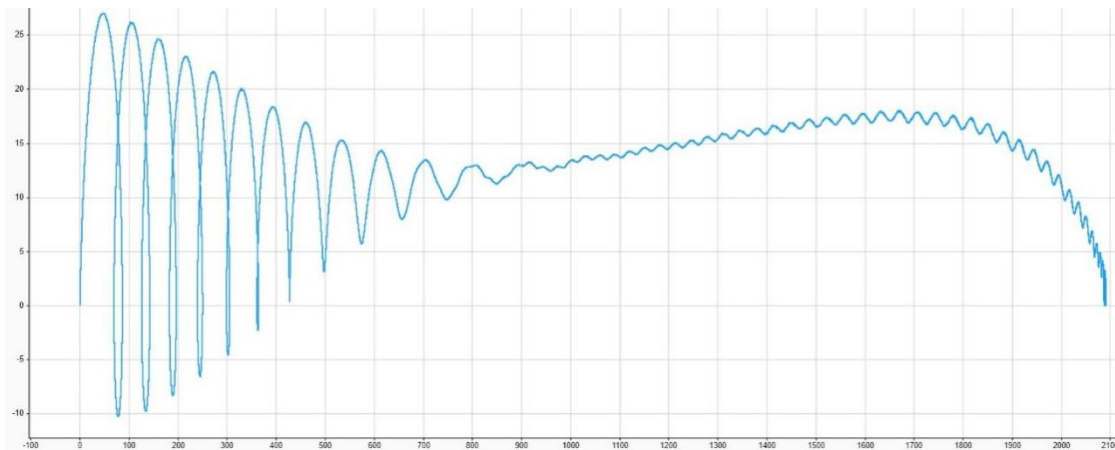


Figure (A)

### 3. CONCLUSION

A simulation model of systems consisting of a multilevel inverter and an induction machine has been developed. A series connection of three-level inverters has been proposed for a medium-voltage SQIM drive with increased voltage capacity. The topology ensured high-power operations with medium-voltage output having several voltage levels. The reduction in the ratings of the dc bus capacitor and reduced imbalance problems in the dc bus are some of the advantages of the proposed topology over the existing topologies. The disadvantage of the proposed topology is that it requires additional output transformers which introduce additional cost and losses. However, these transformers do not have complex underutilized windings like that required in cascaded H-bridge topologies. In this paper conventional and the cascaded multilevel inverter topologies were discussed and results were placed. Finally a Matlab/Simulink model is developed and simulation results are presented.

### REFERENCE

1. F. Wang, "Motor shaft voltages and bearing currents and their reduction in multilevel medium-voltage PWM voltage-source-inverter drive applications," *IEEE Trans. Ind. Appl.*, vol. 36, no. 5, pp. 1336–1341, Sep./Oct. 2000.
2. S. Chen and T. A. Lipo, "Bearing currents and shaft voltages of an induction motor under hard- and soft-switching inverter excitation," *IEEE Trans. Ind. Appl.*, vol. 34, no. 5, pp. 1042–1048, Sep./Oct. 1998.
3. L. M. Tolbert, F. Z. Peng, and T. G. Habetler, "Multilevel converters for large electric drives," *IEEE Trans. Ind. Appl.*, vol. 35, no. 1, pp. 36–44, Jan./Feb. 1999.

4. A. Muetze and A. Binder, "Calculation of circulating bearing currents in machines of inverter-based drive systems," *IEEE Trans. Ind. Electron.*, vol. 54, no. 2, pp. 932–938, Apr. 2007.
5. J. Rodriguez, J. S. Lai, and F. Z. Peng, "Multilevel inverters: A survey of topologies, control and applications," *IEEE Trans. Power Electron.*, vol. 49, no. 4, pp. 724–738, Aug. 2002.
6. P.W. Hammond, "A new approach to enhanced power quality for medium voltage drives," *IEEE Trans. Ind. Appl.*, vol. 33, no. 1, pp. 202–208, Jan./Feb. 1997.
7. R. Teodorescu, F. Blaabjerg, J. K. Pederson, E. Cengelci, and P. N. Enjeti, "Multilevel inverter by cascading industrial VSI," *IEEE Trans. Ind. Electron.*, vol. 49, no. 4, pp. 832–838, Aug. 2002.
8. A. Nabae, I. Takahashi, and H. Akagi, "A new neutral point clamped inverter," *IEEE Trans. Ind. Appl.*, vol. 17, no. 5, pp. 518–523, Sep./Oct. 1981.
9. J.-S. Lai and F. Z. Peng, "Multilevel converters—A new breed of power converters," *IEEE Trans. Ind. Appl.*, vol. 32, no. 3, pp. 509–517, May/Jun. 1996.
10. G. Cararra, S. Gardella, M. Marchesoni, R. Salutari, and G. Sciutto, "A new multilevel PWM method: A theoretical analysis," *IEEE Trans. Power Electron.*, vol. 7, no. 3, pp. 497–505, Jul. 1992.
11. A.M. Trzynadlowski, R. L. Kirlin, and S. Legowski, "Space vector PWM technique with minimum switching losses," *IEEE Trans. Ind. Electron.*, vol. 44, no. 2, pp. 173–181, Apr. 1997.
12. Y. S. Lai and S. R. Bowes, "Optimal bus-clamped PWM techniques for three-phase motor drives," in *Proc. Annu. Conf. IEEE Ind. Electron. Soc.*, Busan, Korea, Nov. 2–6, 2004, pp. 1475–1480.
13. Suvajit Mukherjee and Gautam Poddar "A Series-Connected Three-Level Inverter Topology for Medium-Voltage Squirrel-Cage Motor Drive Applications" *Ieee Transactions On Industry Applications*, Vol. 46, No. 1, January/February 2010.